

# ISTC project K-1265:

## **Experimental study of core melt in-vessel retention IN-VEssel COrium Retention (INVECOR)**

Presented by Vladimir Zhdanov  
IAE NNC RK

CEG-SAM 11<sup>th</sup> Meeting,  
March, 6 – 9, 2007  
Dresden, Germany

# Presentation contents

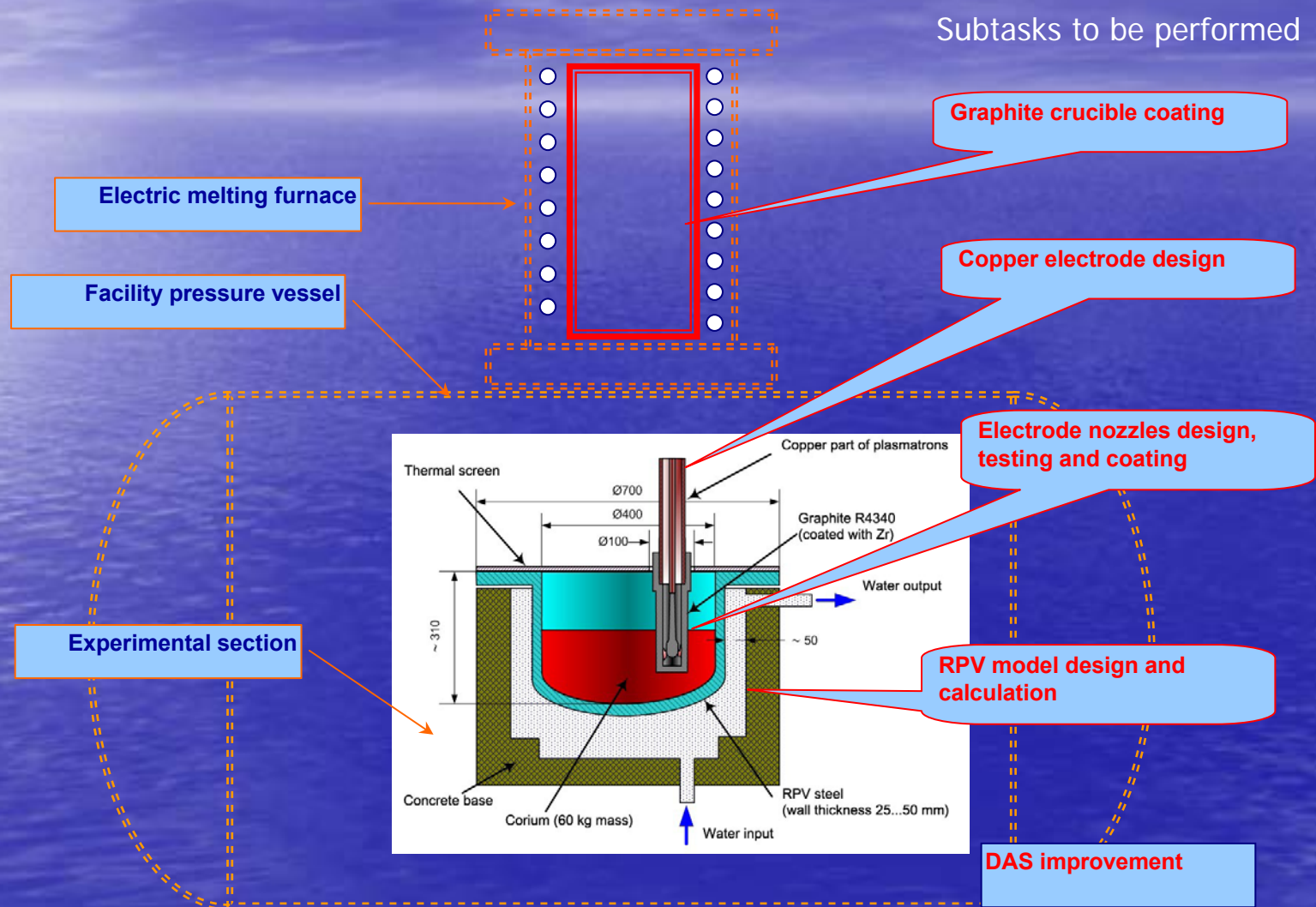
- Introduction
- Main directions of work and results
  - ❑ Testing of Zr-coating technique on large scale crucible inner surface
  - ❑ Check of some phenomena of molten zirconium behavior in small-scale experiments
  - ❑ Design and testing of device for decay heat modeling (DDHM)
  - ❑ Test section (TS) design (RPV model)
  - ❑ Small scale test for engineered estimate of RPV model design
  - ❑ Pre-calculation of above items
- Conclusions

# Introduction

- Project K-1265 has been started from May 1, 2006.
- Operations are fulfilled according to the confirmed Working Plan (for today while there are no terminated operations).
- Ongoing task are:
- Modernization of test facilities, optimization of melting process and simulation of decay heat.
- Calculation support of experiments.
- Post-test analysis.
- Requests for procurement of materials and equipment were sent to ISTC office. Most units of equipment are delivered in IAE.



# Major directions of LAVA-B facility modernization

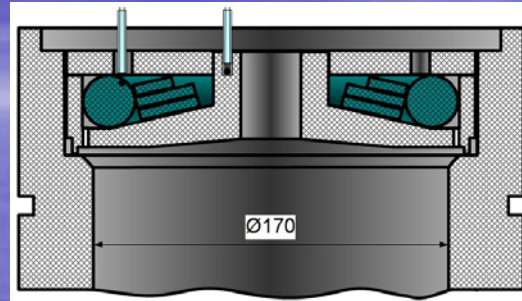
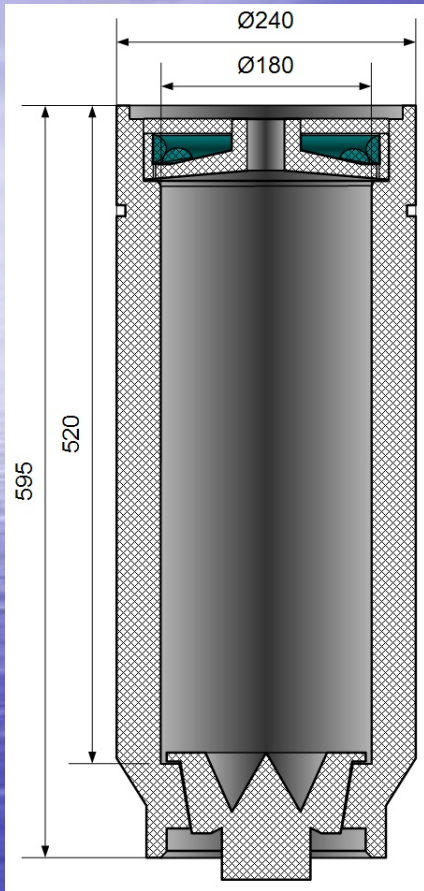


# Tests of Zr-coating of large scale crucible

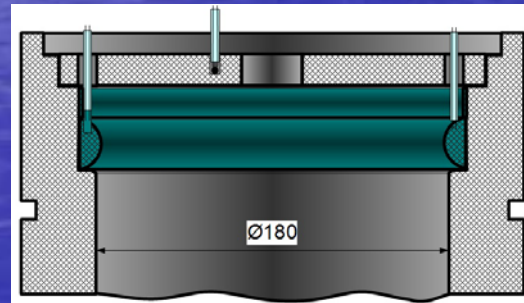
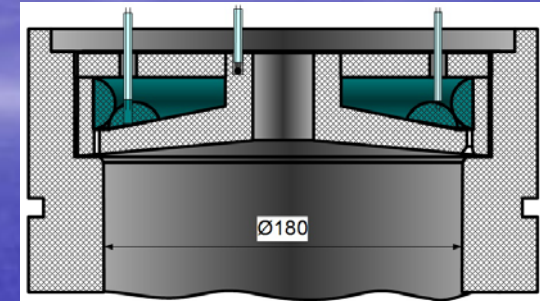
Main differences in heating conditions of large-scale crucible compared with small-scale crucible are:

- Presence of temperature gradient along the crucible height
- Very long process of crucible cooling due to big thermal capacity of graphite materials
- Presence of impurities in the gas medium because of presence of a plenty of porous materials in EMF ( $O_2$ ,  $N_2$ )

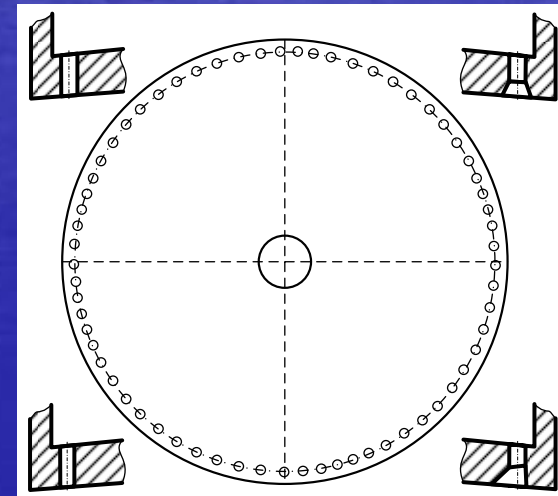
# Tests of Zr-coating of large scale crucible



1<sup>st</sup> test



3<sup>rd</sup> test

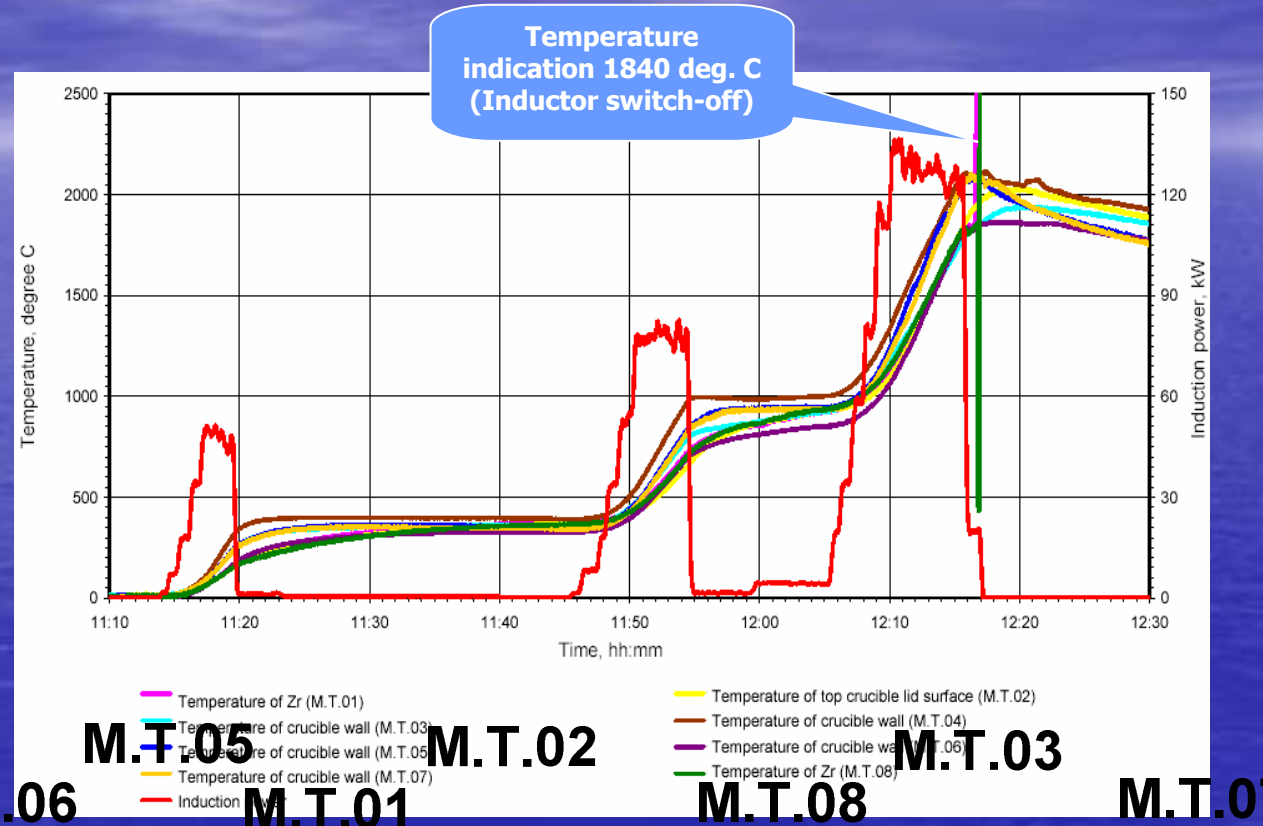
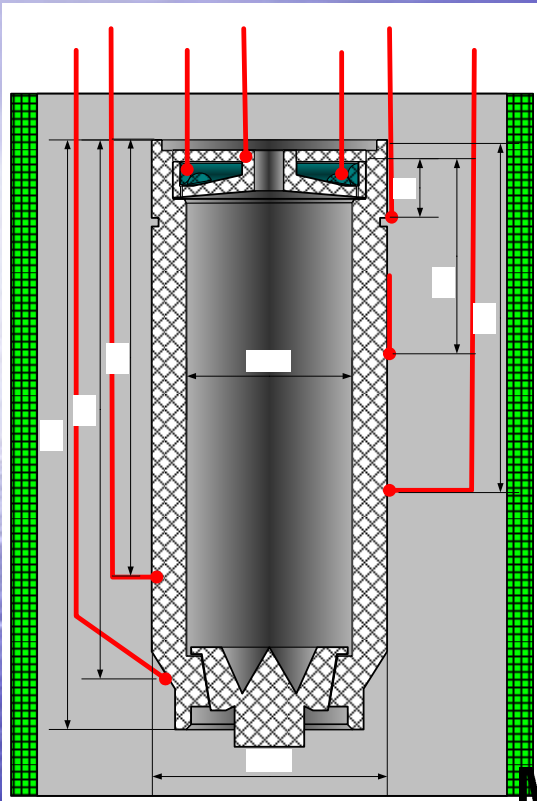


2<sup>nd</sup> test

Variants of zirconium initial loading in the crucible

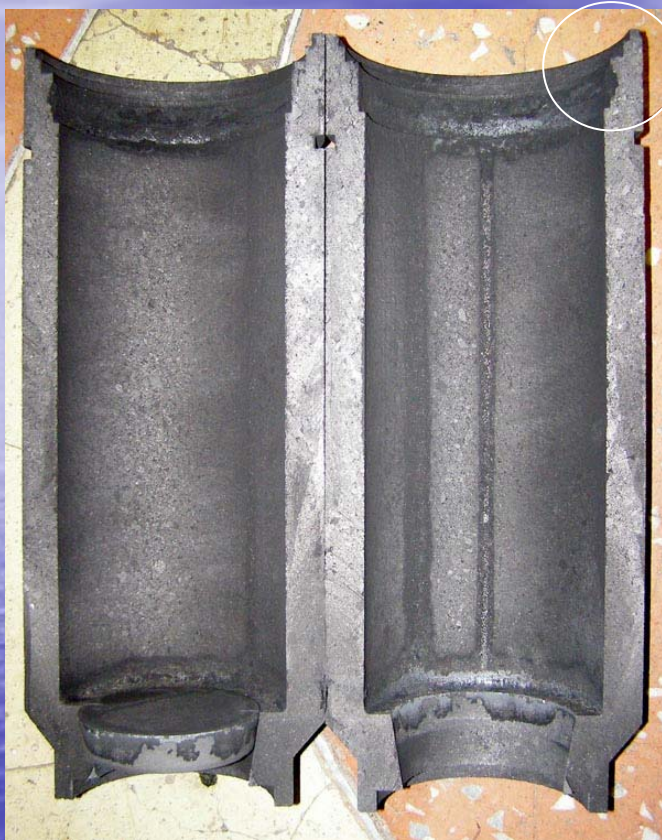


# Tests of Zr-coating of large scale crucible



Temperature history of large scale crucible coating (2<sup>nd</sup> test)

# Tests of Zr-coating of large scale crucible



3<sup>rd</sup> test

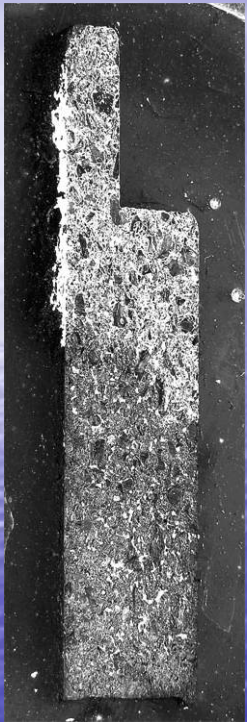


2<sup>nd</sup> test

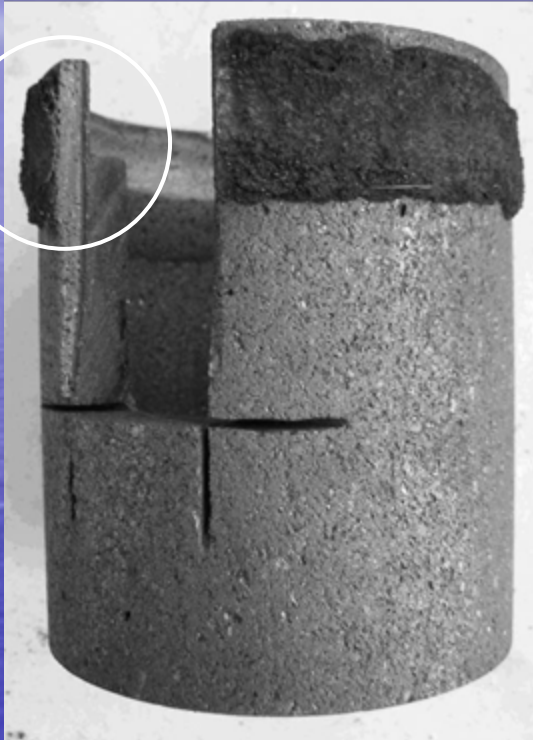
Results of large scale crucible coating (2<sup>nd</sup> test)



# Small-scale tests on Zr-coating with graphite of different porosity



GMZ-graphite  
(porosity >26%)



ARV-graphite  
(Porosity <18%)



# Summary to crucible protection

- Use of graphite with high porosity leads to deep penetration of molten zirconium into crucible wall (up to appearance of zirconium on the outer surface of the crucible)
- Application of graphite with lower porosity allows to obtain the thin film of zirconium on the inner surface of crucible
- It is effectually to use the crucibles with conical inner surface for providing of slow droop of initial zirconium ring as it melt
- Testing of Zr-coating will be continued after receiving of isostatic graphite made in SGL Carbon Group (Germany) with porosity less than 12%
- Idea of conical inner surface of crucible will be tested in small-scale facility

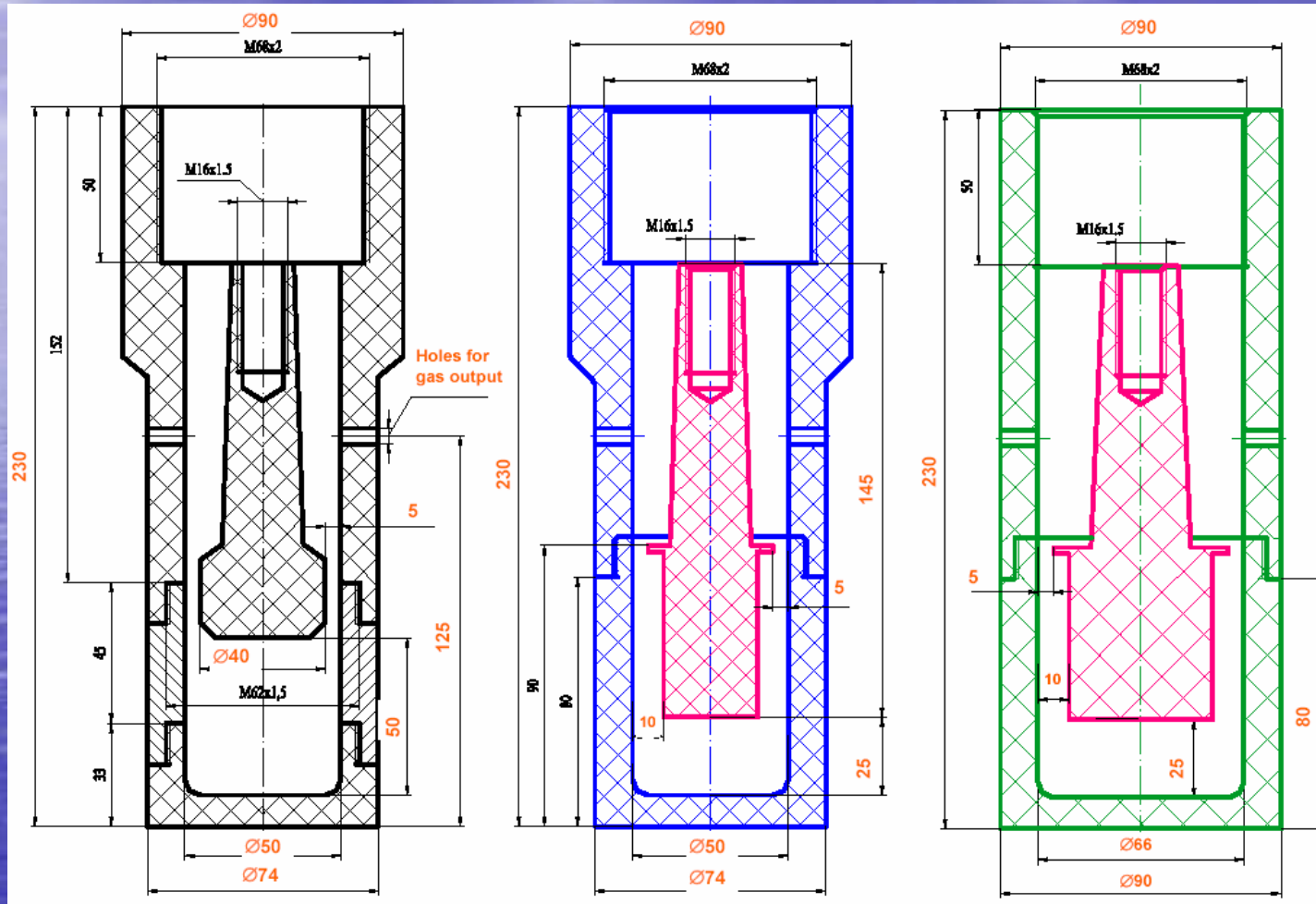


# Device for decay heat modeling

- Designing of new plasmatrons is under way (in the concept of new plasmatrons the forced movement of an arc in an azimuth direction and magnification of a resource of nozzles is included). New variants of plasmatrons design are making under sketches and testing for check-out and an improvement of the concept.
- Development of zirconium coating technique on the outer electrode outer surface is under way. Necessary equipment is made and tested.



# Concepts of electrode design

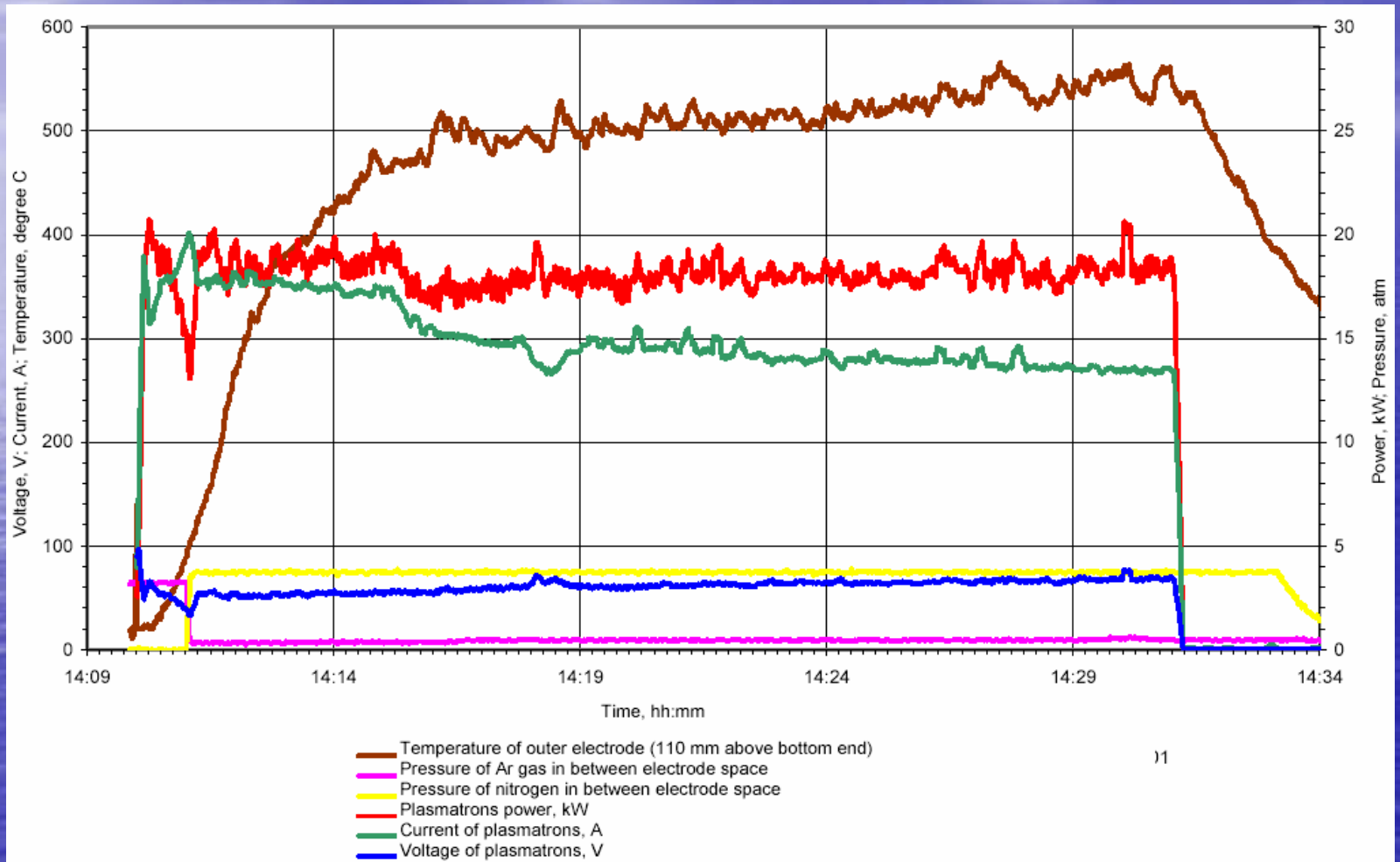


Tested

Tested

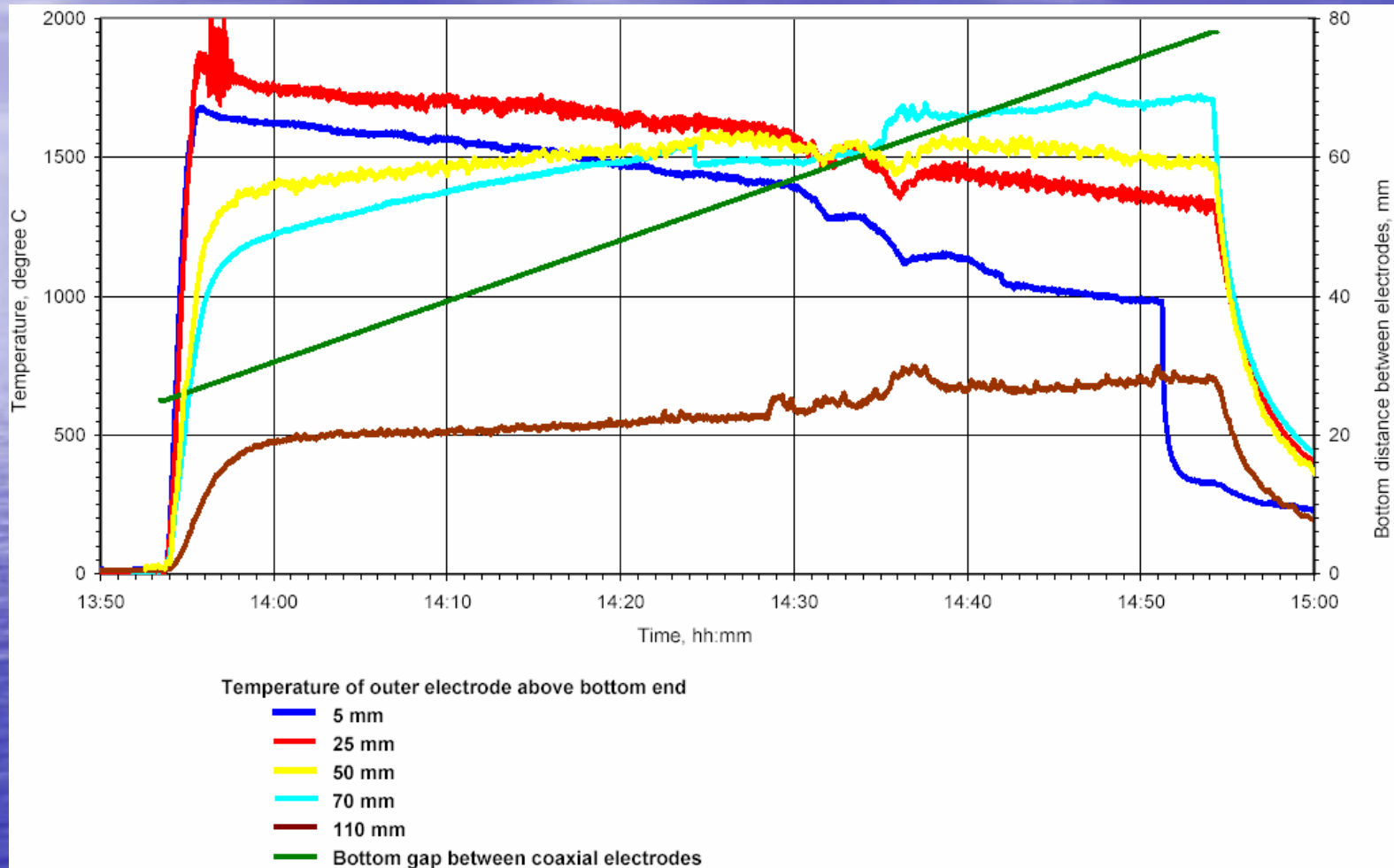
Testing is under way

# Testing of composite electrode nozzles



Test parameter variation (30 minutes)

# Testing of composite electrode nozzles



Test parameter variation (60 minutes)



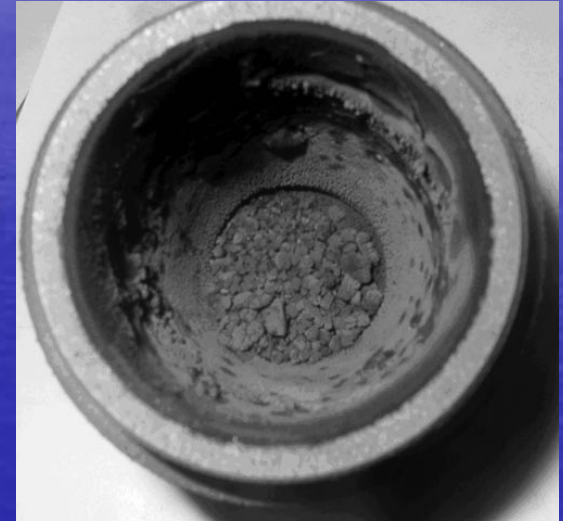
# Testing of composite electrode nozzles



Outer electrode  
3 parts variant



Inner electrode



Outer electrode  
2 parts variant

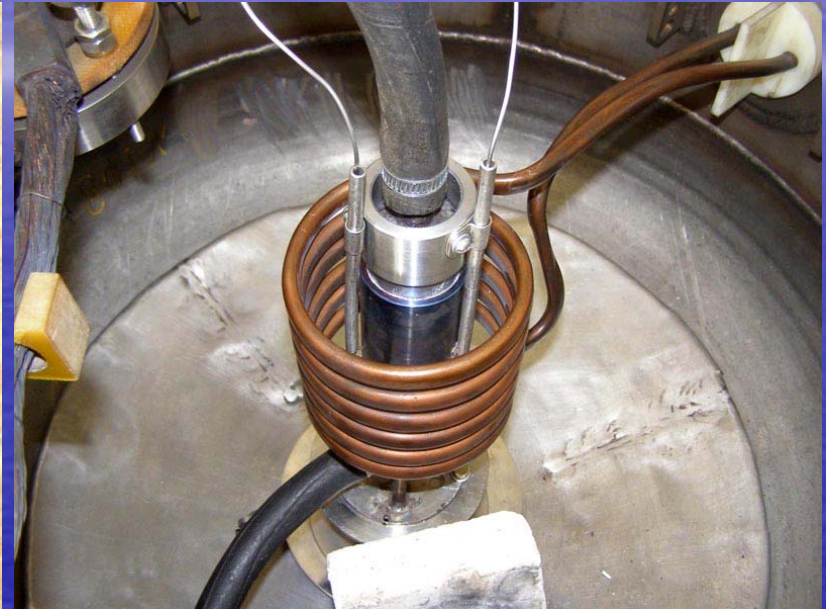
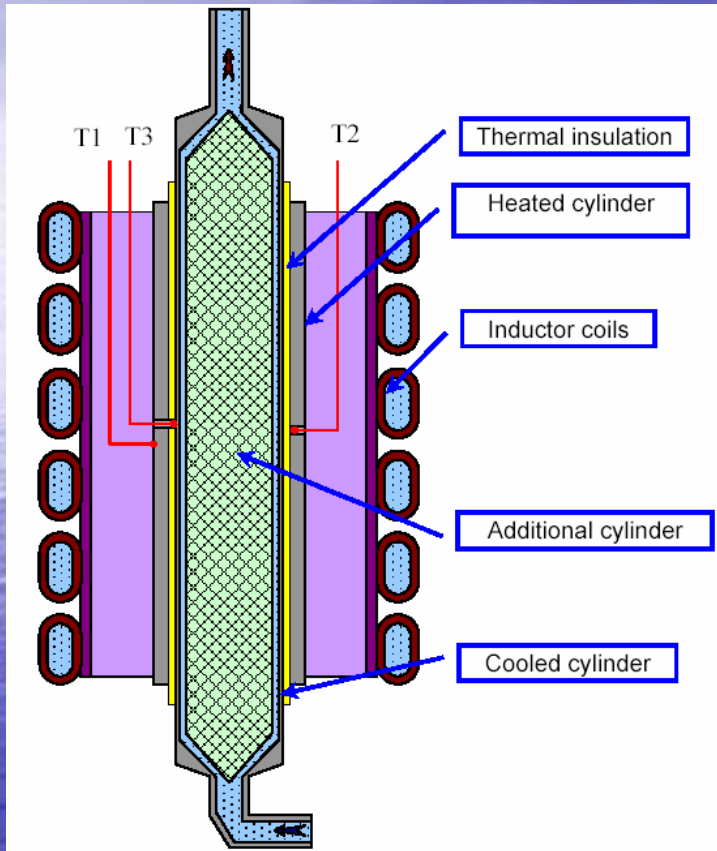
Electrodes view after 1 hour testing

# Test section (RPV model)

- The shape and dimension of RPV model are finally chosen.
- It was solved to make RPV model from usual carbon steel (matrix) and insert the samples of RPV steel into the matrix wall in chosen points.
- Samples of RPV steel will be equipped with thermocouples for different dept.
- Design of samples fixing in the matrix is under way.
- Both part of test sections were requested for procurement.
- Necessity of thermal insulation on the test section outer surface will be discussed.



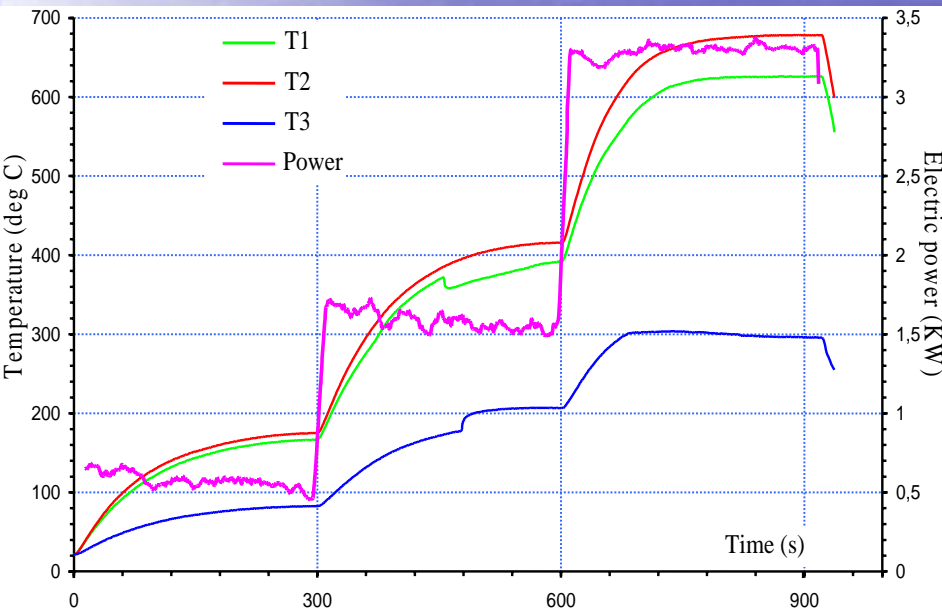
# Test section (RPV model)



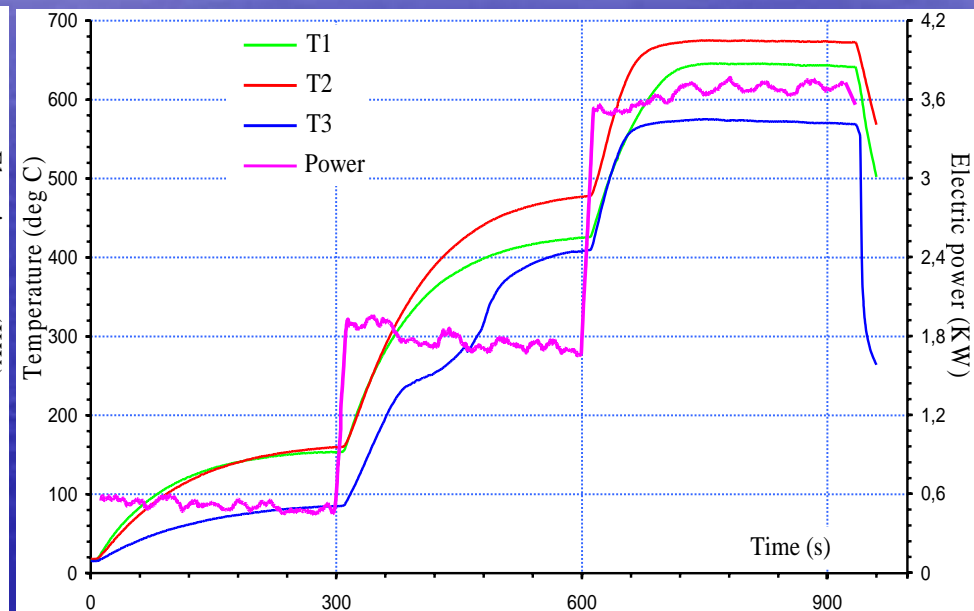
Small-scale test for estimation of thermal flux



# Test section (RPV model)



Glass fabric



Graphite fabric

Test parameters history

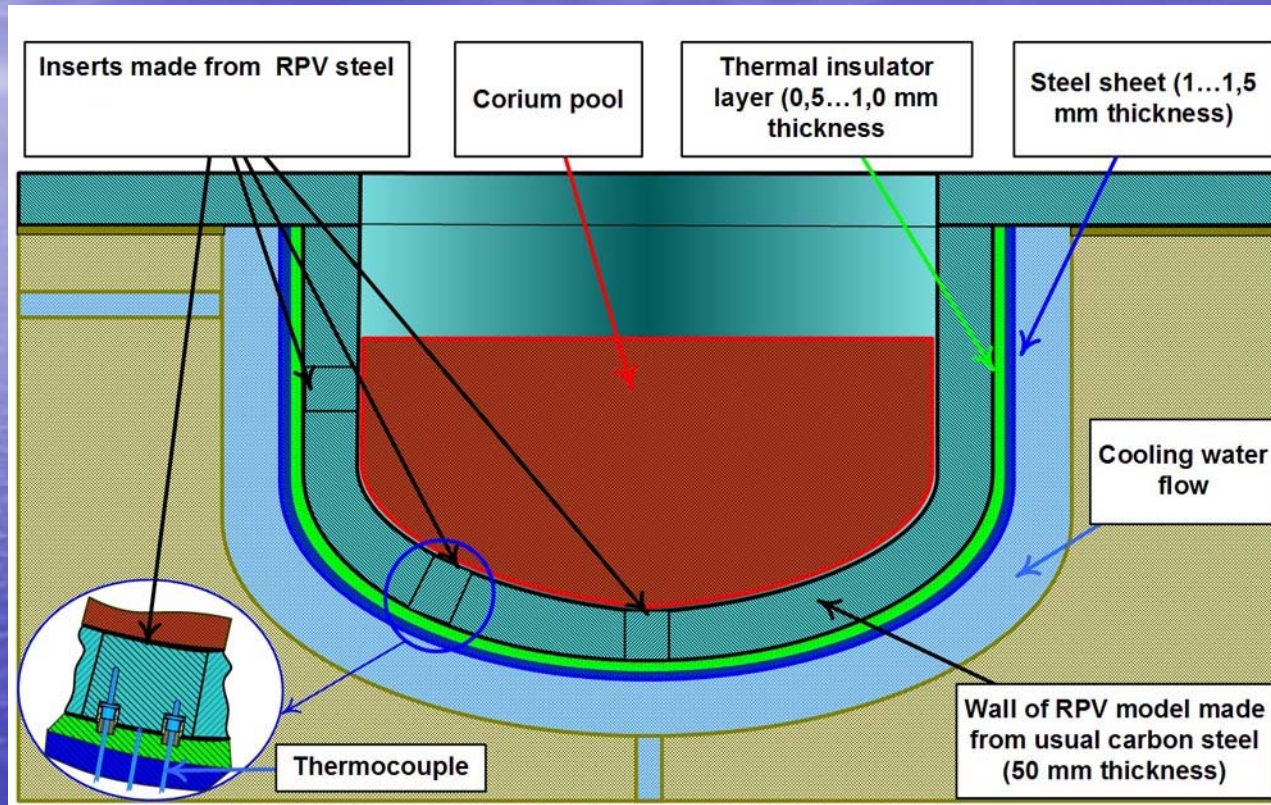
# Test section (RPV model)

(small-scale test parameters)

Parameter	K2	K3	K4
Open flow area of calorimeter, $S_p$ , mm <sup>2</sup>	486,7	486,7	486,7
Dimension of heated cylinder, $d_{in} \times d_{ex} \times h$ ,	40×46×100	40×46×100	40×46×100
Water flow rate, Q, liter/s	0,208	0,208	0,208
Inductor coil diameter, D, mm	95	95	95
Average water temperature, degree C	~16	~16	~16
Thermal insulation	Glass fabric	Glass fabric	Graphite fabric
Thickness of thermal insulation, mm	0,32	0,32	0,5
Maximum temperature difference (T2-T3), K	380	386	102



# Test section (RPV model)

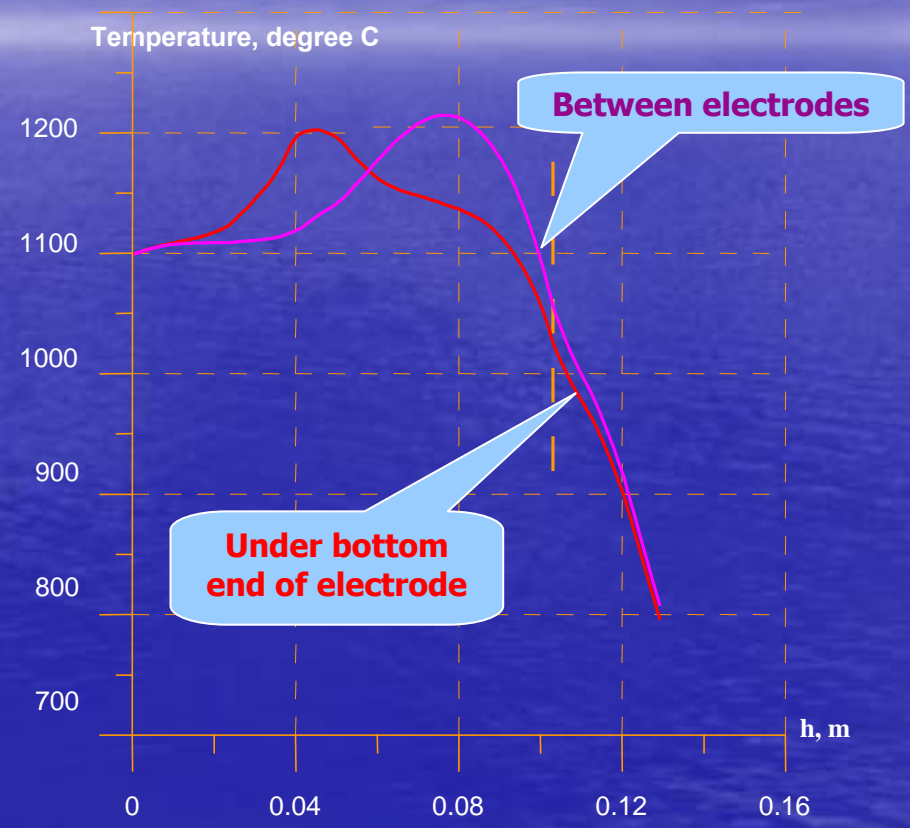
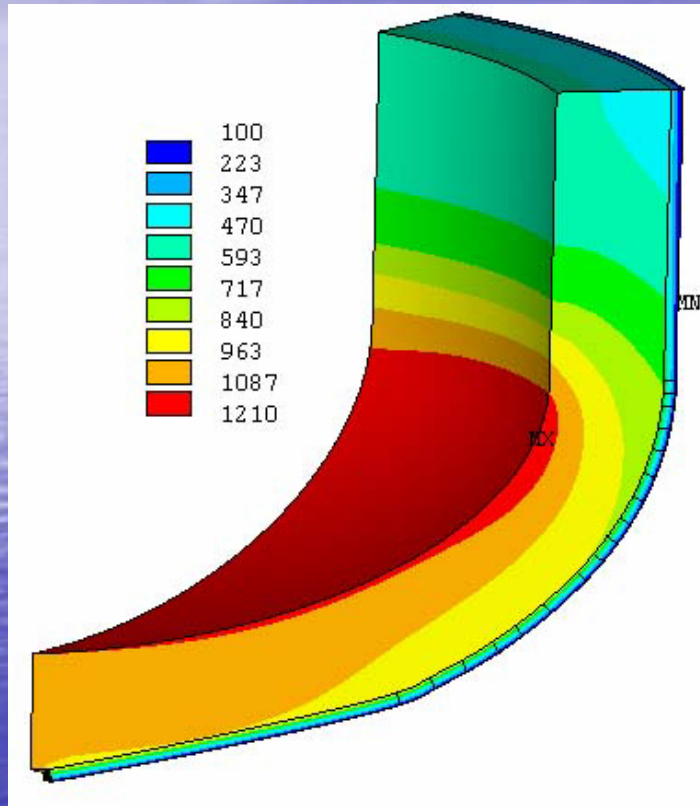


Possible design of RPV model



# Test section (RPV model)

Corium pool pre-calculation using profile thermal insulation on the outer RPV model surface

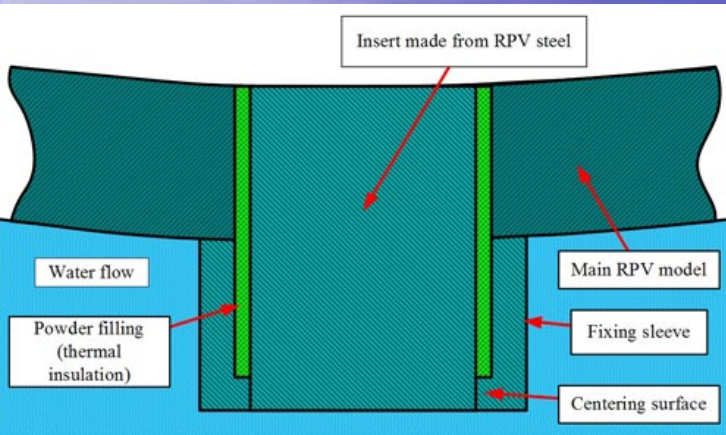


$H_{CT} = 45 \text{ mm}$

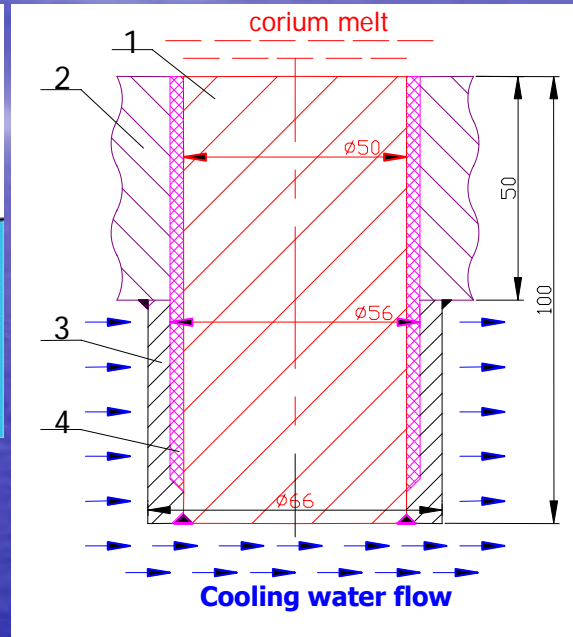
Thermal insulation  $\lambda/\delta = 100$  on the length from center  $\sim 120 \text{ mm}$

Thermal insulation  $\lambda/\delta = 200$  on the other surface

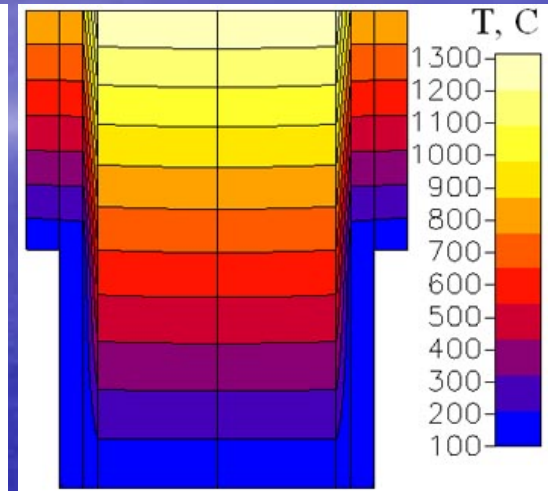
# Test section (RPV model)



Scheme of design



Scheme for calculation



Temperature field in RPV insert for condition:

$$\lambda_{\text{steel}} = 30 \text{ W/m} \cdot \text{K}$$

$$\lambda_{\text{ZrO}_2} = 0.1 \text{ W/m} \cdot \text{K}$$

$$q_{\text{corium}} = 4.25 \text{E}5 \text{ W/m}^2$$

$$T_{\text{water}} = 100 \text{ degree C}$$

Possible design of RPV steel insert  
(without thermal insulation on outer surface of RPV model)



# Conclusions

- Basic works of project Working Plan are under way
- Several test in large scale facility were performed for elaboration of Zr-coating technique on the large scale crucibles (using available crucibles made from porous graphite).
- Effect of graphite porosity on molten zirconium spreading was tested in small-scale facility.
- Testing of heater for molten corium is continued and new electrodes design is developed.
- New concept of RPV model was developed. Possibility of temperature increase on the inner surface of RPV model was tested using small-scale facility.
- Pre-calculation of corium pool for new experimental section concept was performed.
- Technique development of Zr- coating application on large scale crucible and electrode nozzles is under way
- Data acquisition system improvement is performed during current tests performance